

Ion Energy Distribution Measurements Past, Present and Future

(*Focus on Retarding Field Analyser Technology*)

David Gahan CTO

S. Sharma PhD candidate, Mike Hopkins CEO



Talk Outline

Past

- The Ion Energy Distribution Function (IEDF)
- Retarding Field Analyser (RFA)
 - IEDF of IVDF?
- Previous state of the art in RFA Technology

Present

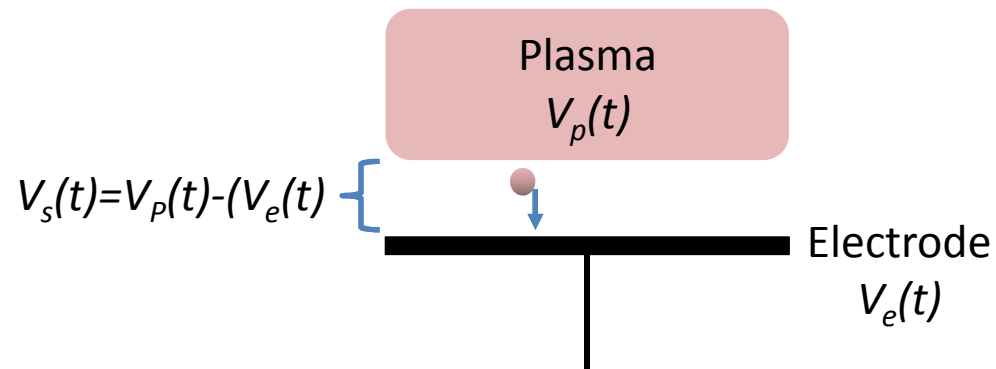
- Recent advances in RFA Technology
 - Floating RFAs for (rf) biased electrodes
 - Pulsed rf and time resolved functionality
 - RFA with spatial resolution
 - Ion Angular Distribution measurement

Future

- RFAs with ion mass resolution
- Wireless sensors

The Ion Energy Distribution Function

- Shape of IEDF determined by:
 - sheath potential $V_s(t)$
 - ion transit time τ_i
 - period of sheath potential waveform τ_{rf}



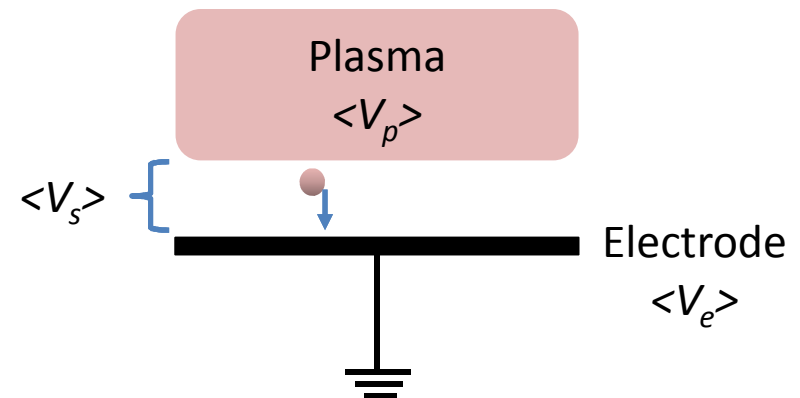
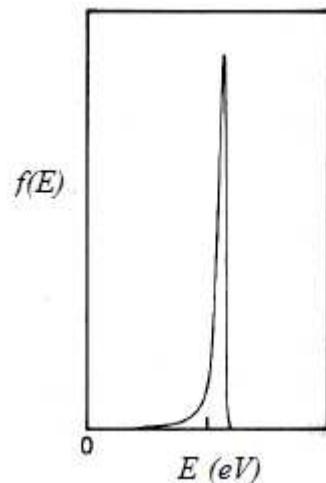
The Ion Energy Distribution Function

- For DC sheath

- $\langle E \rangle \rightarrow \langle eV_s \rangle$

- $\Delta E \rightarrow 0$

- FWHM 2 – 3eV



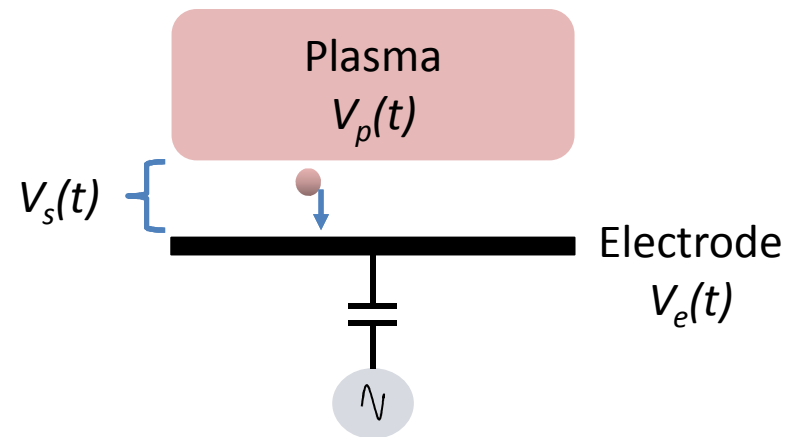
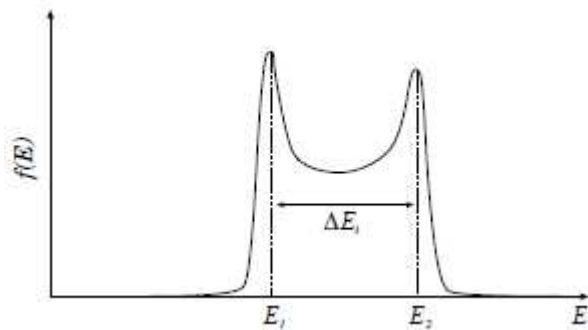
The Ion Energy Distribution Function

- For RF sheath

- Ion transit time $\tau_i = 3\bar{s} \sqrt{m_i / (2e\bar{V}_s)}$

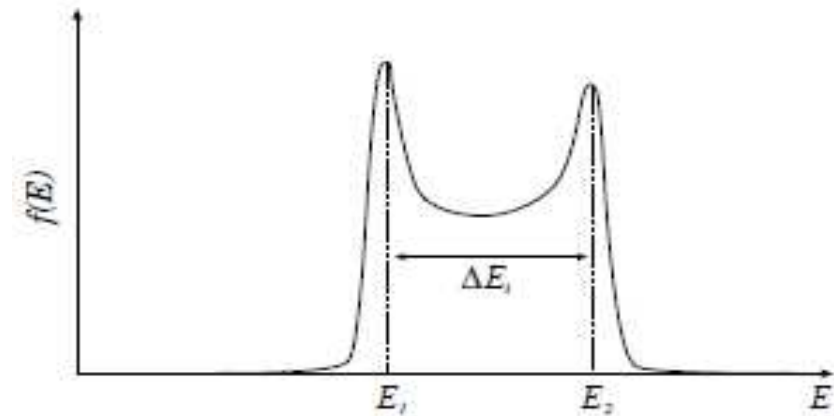
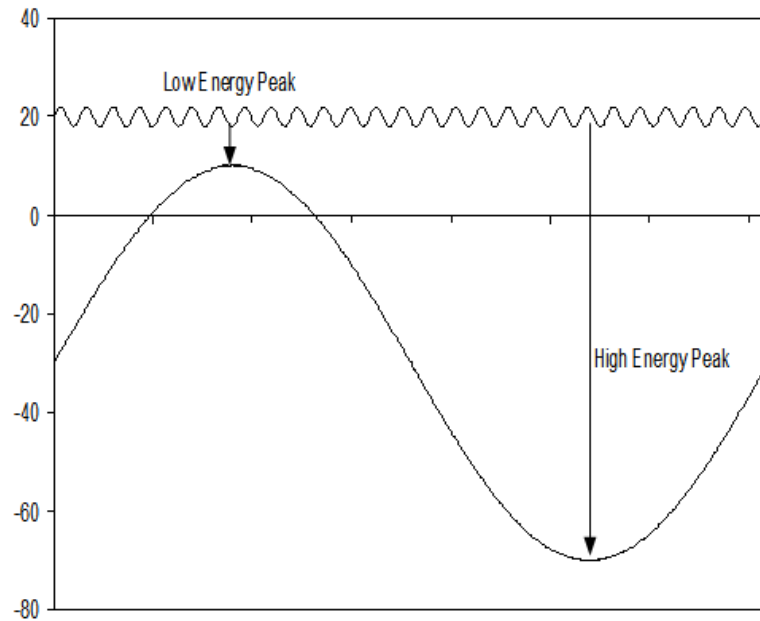
- $f(E) = \frac{dn}{dE} = \frac{2n_i}{\omega \Delta E_i} \left[1 - \frac{4}{\Delta E_i^2} (E - e\bar{V}_s)^2 \right]^{-1/2}$

- $\Delta E = \frac{4e\bar{V}_s}{\pi} \left(\frac{\tau_{rf}}{\tau_i} \right)$



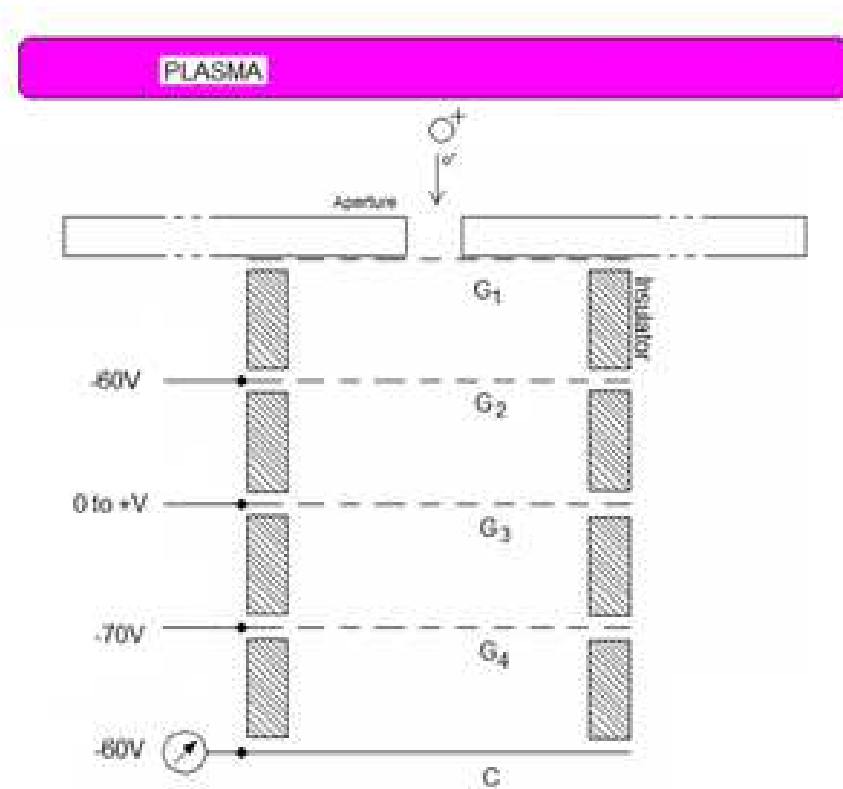
Benoit-Cattin P, Bernard L C and Bordenave-Montesquieu A
 1967 Dispersion en énergie des ions produits par une
 source à excitation de haute fréquence *Entropie* 18 29

The Ion Energy Distribution Function



The Retarding Field Analyser (RFA)

- Planar, Gridded Structure
- G1 prevents plasma entering RFA
- G2 repels plasma electrons
- G3 retards ion flow
- G4 prevents secondary emission from C
- C collects current of ions



The Retarding Field Analyser (RFA)

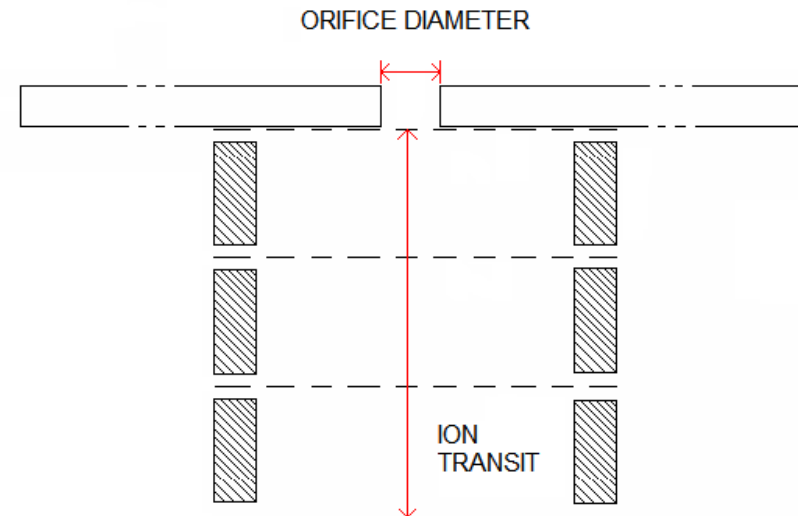
- Orifice diameter < Debye length λ_D

- $\lambda_D = \left(\frac{\epsilon_0 k T_e}{n_e e^2} \right)^{1/2}$ e.g. $T_e = 3\text{eV}$, $N_e = 10^{17}\text{m}^{-3}$ $\lambda_D \sim 40\mu\text{m}$

- Ion transit length < Ion mean free path λ_i

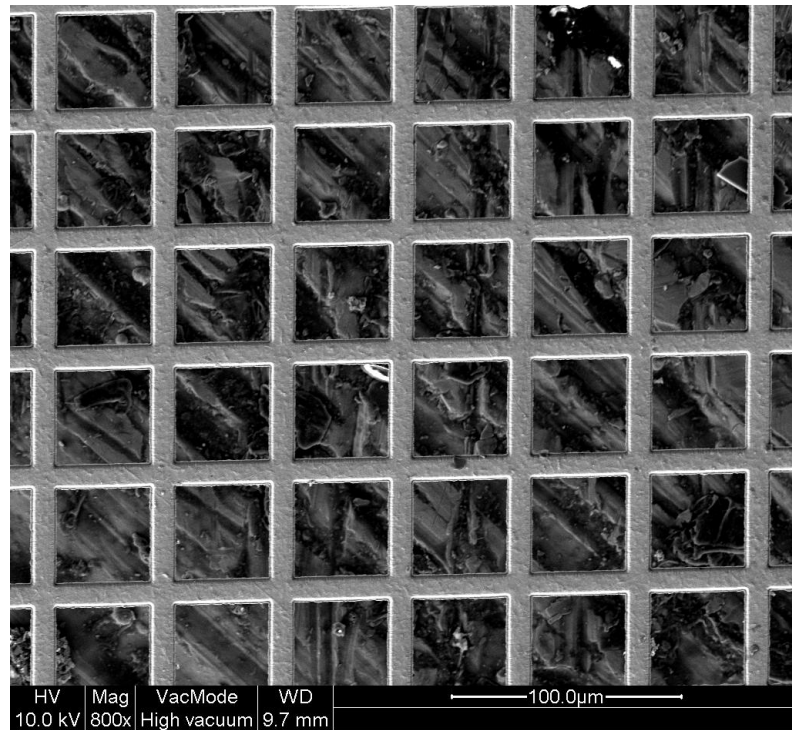
- $\lambda = \frac{1}{\sigma n}$

- RFEA depth 0.8mm ~ 100mTorr in Argon

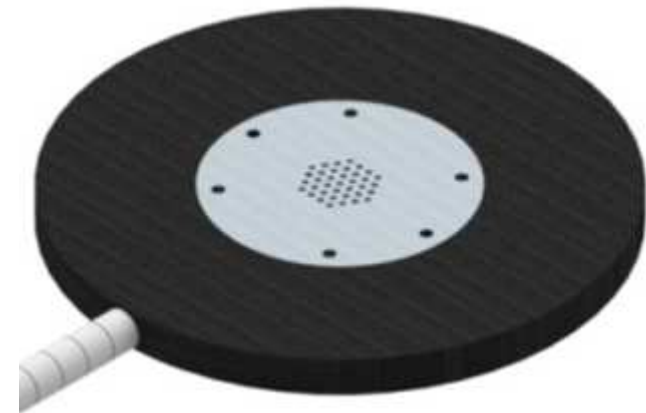


The Retarding Field Analyser (RFA)

Nickel Grid

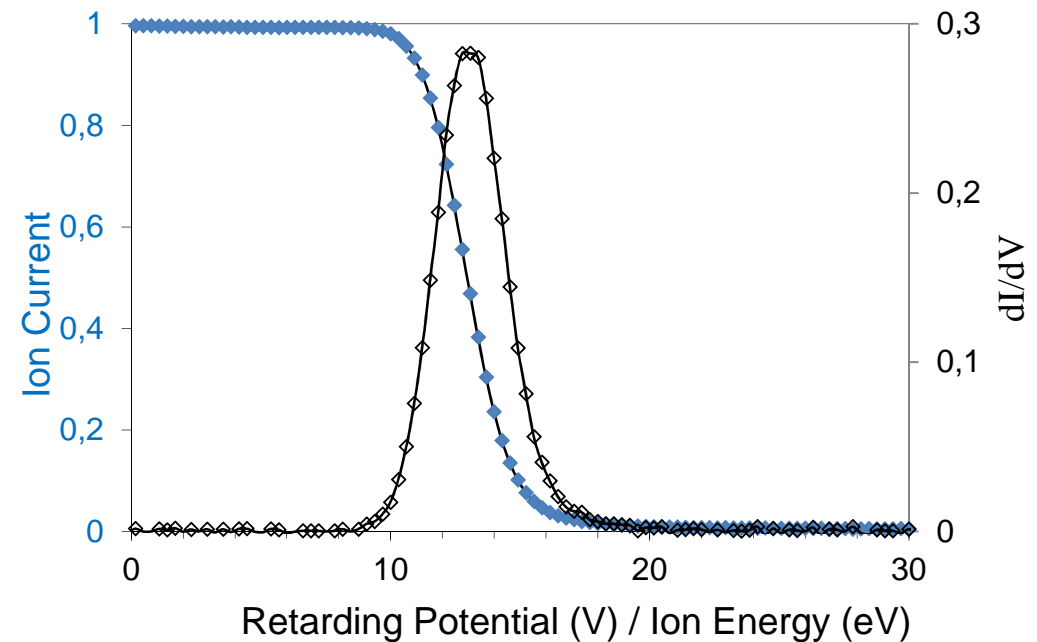


RFA



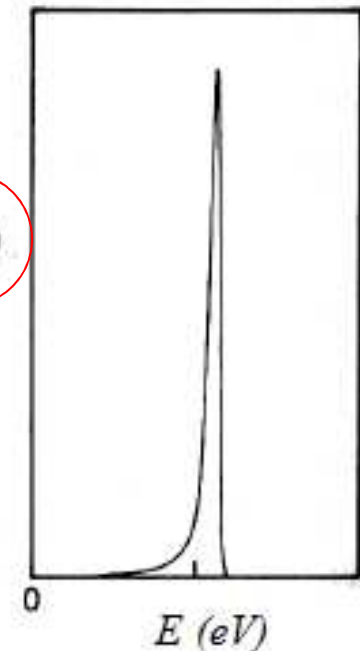
The Retarding Field Analyser (RFA)

- Ion Energy = eV_{G2}
- $f(E) = dI_c / dV_{G2} ??$

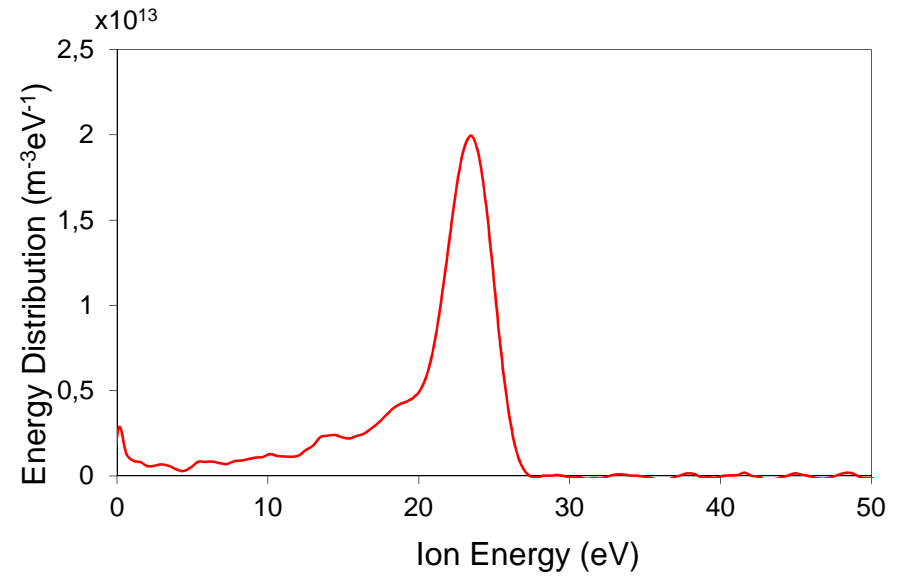
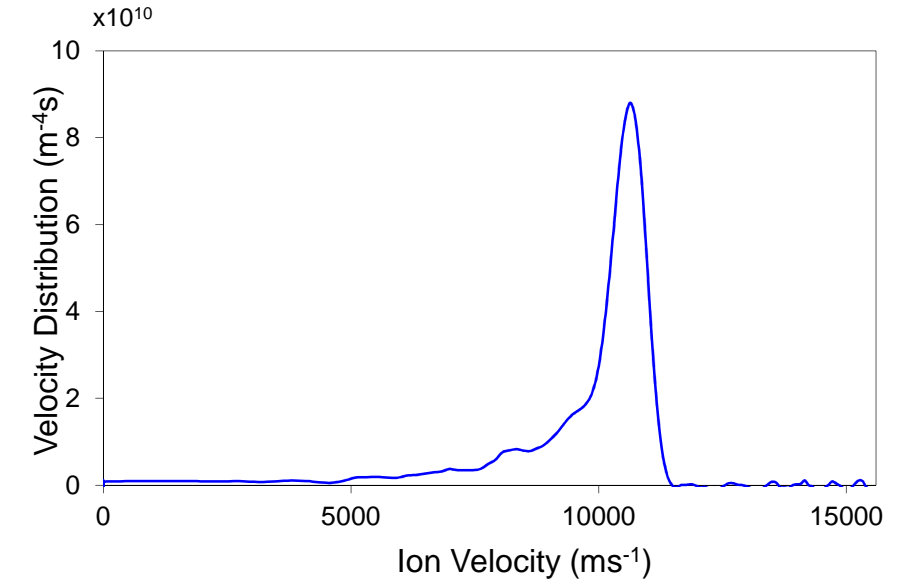
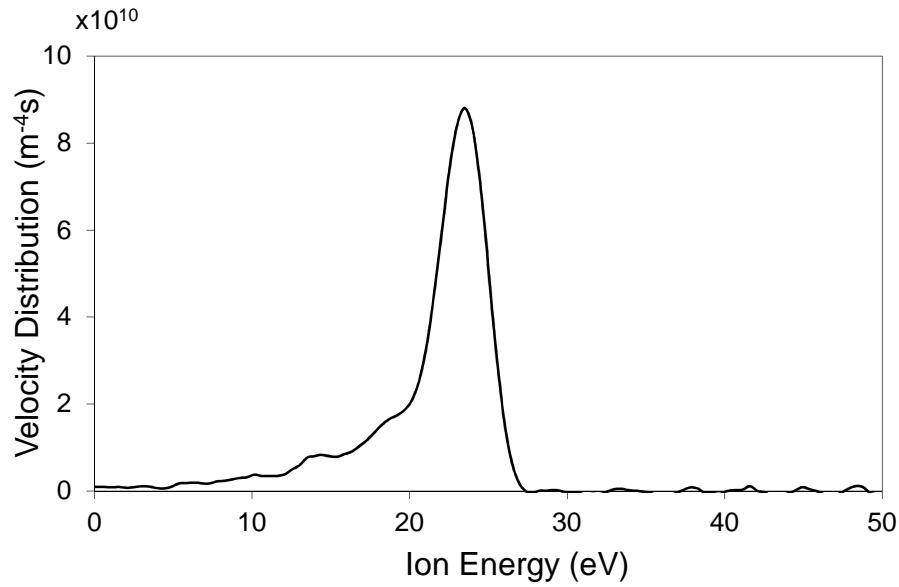


IVDF or IEDF??

- Ion Energy distribution function
 - Variable on Y axis must be a function of E
- $dI_c/dV_{G2} = f(E) ??$
- $I_c \propto nev$
 - $v = (2E/m)^{1/2}$
 - $\therefore I_c \propto (E/m)^{1/2}$
 - $dI_c/dV_{G2} = f((E/m)^{1/2}) = f(v) = \text{IVDF}!!$
- RFA gives IVDF versus Energy

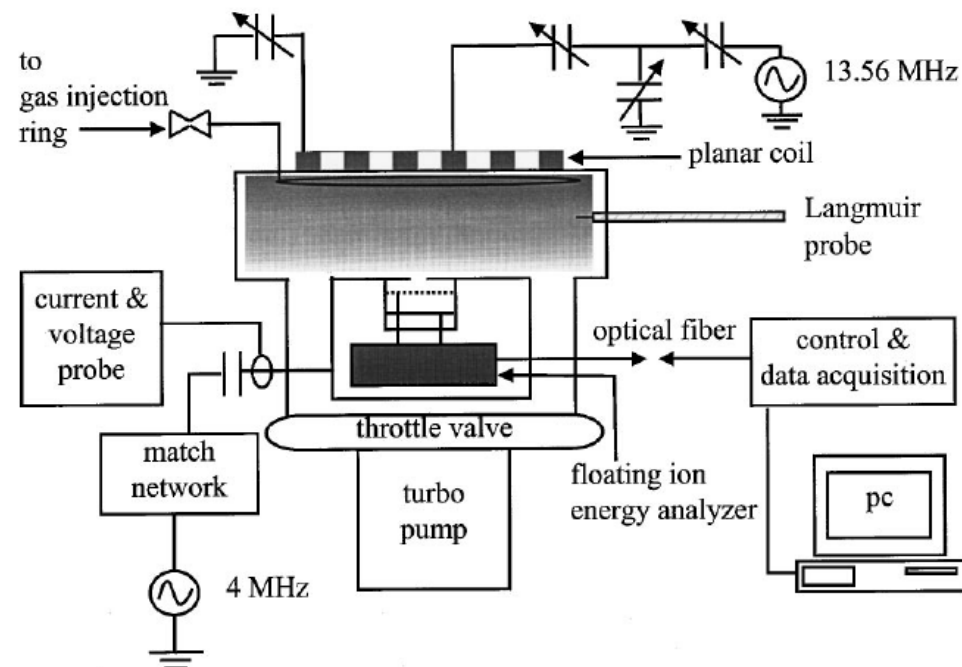


IVDF or IEDF???



Previous State of the Art

- Previous state of the art
- Disadvantages:
 - Complex electronics
 - Redesign of rf chuck
 - Not commercially viable as instrument



REVIEW OF SCIENTIFIC INSTRUMENTS

VOLUME 70, NUMBER 6

JUNE 1999

Compact floating ion energy analyzer for measuring energy distributions of ions bombarding radio-frequency biased electrode surfaces

Erik A. Edelberg
Department of Chemical Engineering, University of California Santa Barbara, Santa Barbara, California 93106

Andrew Perry and Neil Benjamin
Lam Research Corporation, 4650 Cushing Parkway, Fremont, California 94538-6470

Eray S. Aydi[®]
Department of Chemical Engineering, University of California Santa Barbara, Santa Barbara, California 93106

PESM 14

Impedans
Plasma Measurement

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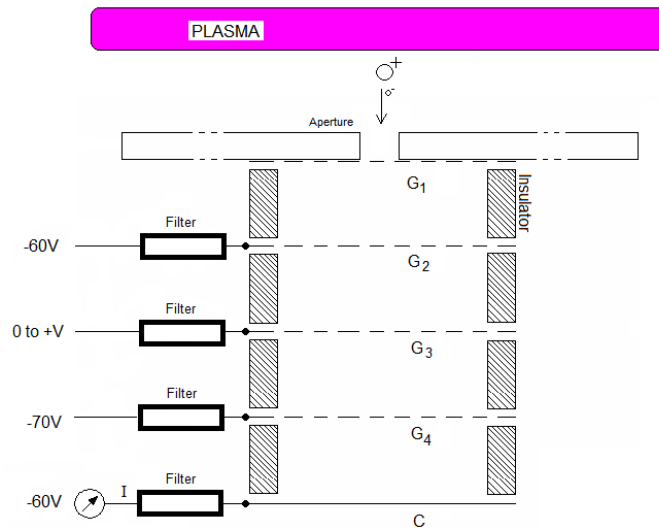
- Recent advances in RFA Technology
 - Floating RFAs for (rf) biased electrodes
 - Pulsed rf and time resolved functionality
 - RFA with spatial resolution
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Future

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- Wireless sensors

Recent Advances in RFA Technology

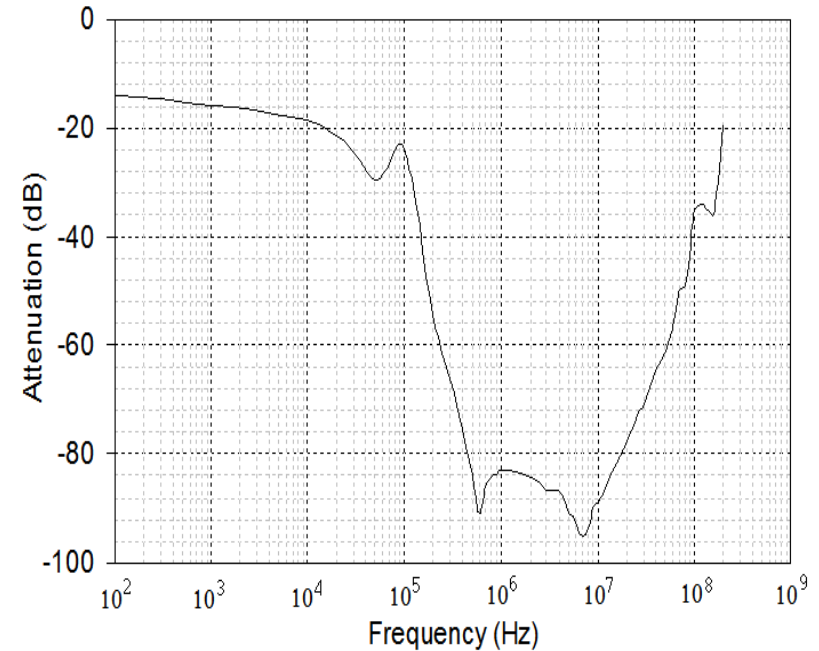
- RFA design compatible with rf biased electrode



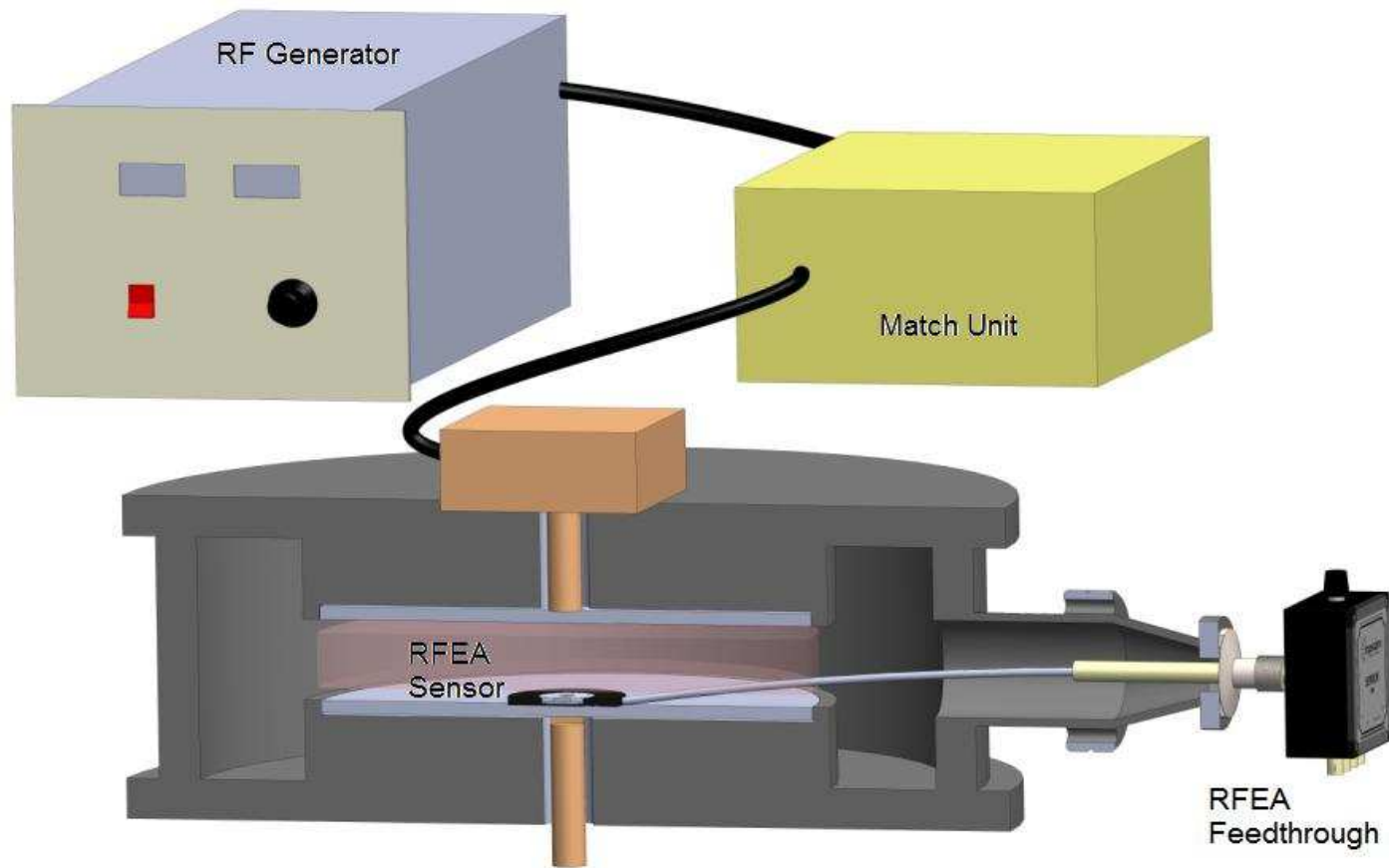
REVIEW OF SCIENTIFIC INSTRUMENTS 79, 033502 (2008)

Retarding field analyzer for ion energy distribution measurements at a radio-frequency biased electrode

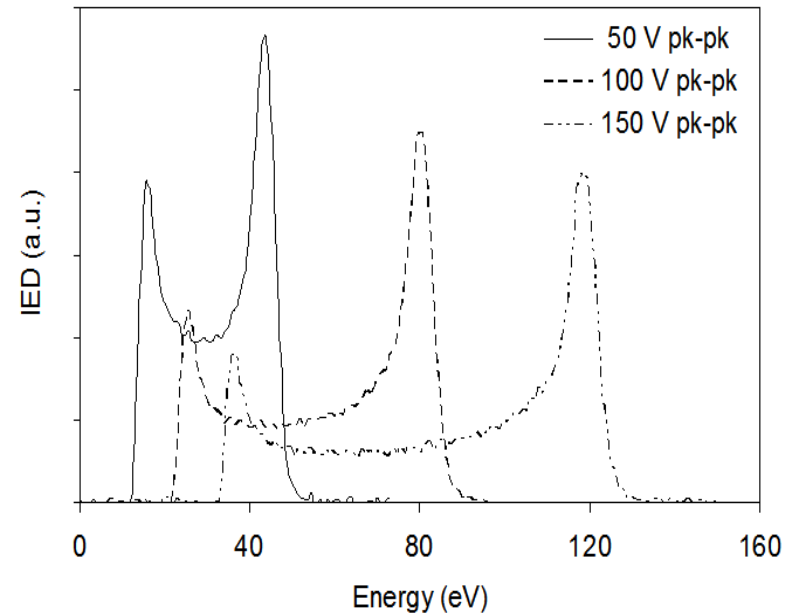
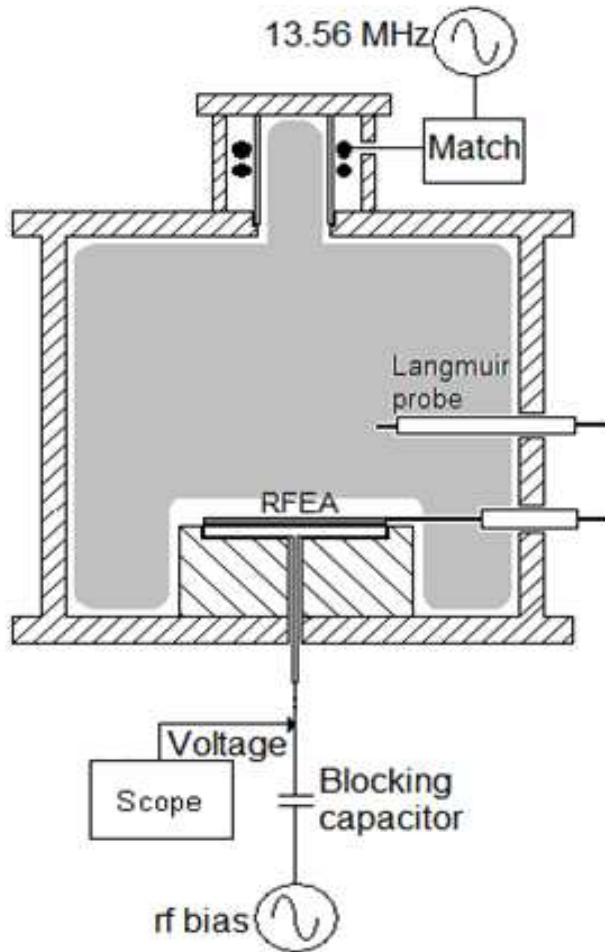
D. Gahan, B. Dolinaj, and M. B. Hopkins



Typical installation

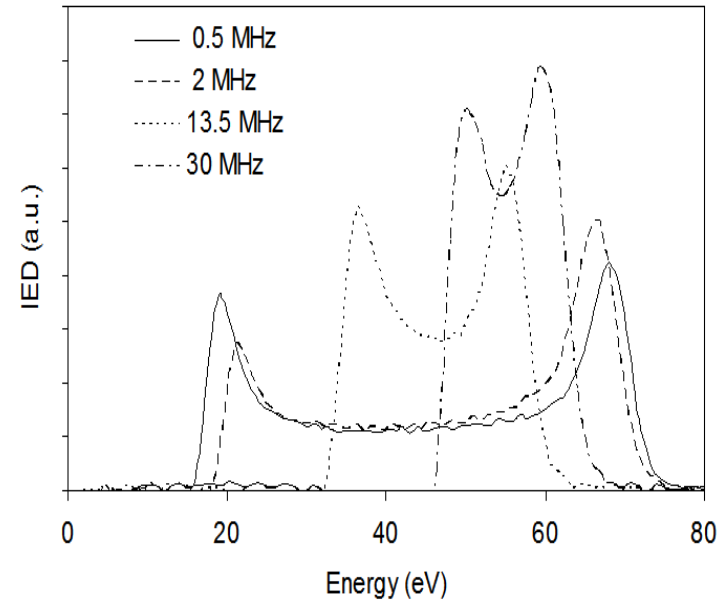
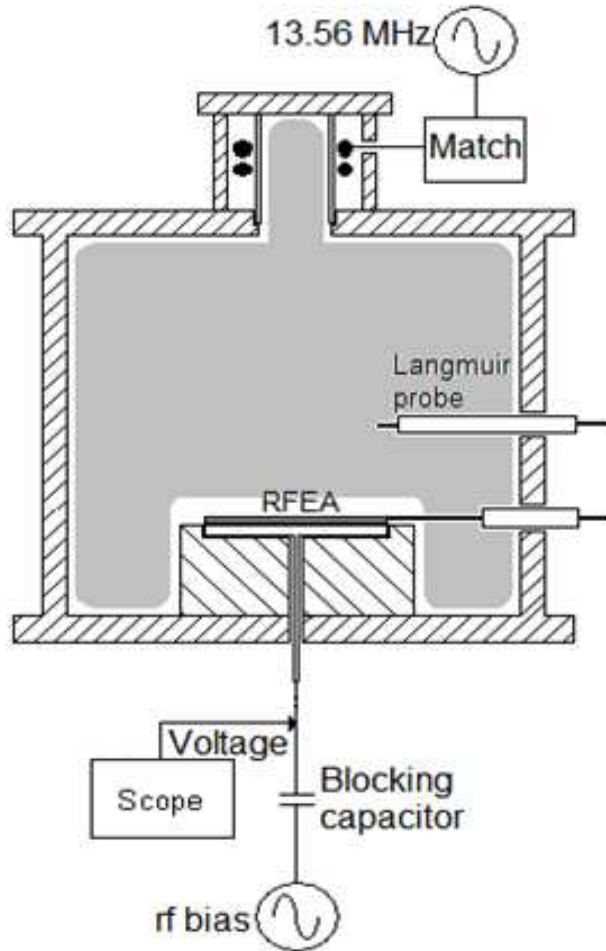


Typical results



$$\Delta E = \frac{4e\tilde{V}_s}{\pi} \left(\frac{\tau_{rf}}{\tau_i} \right)$$

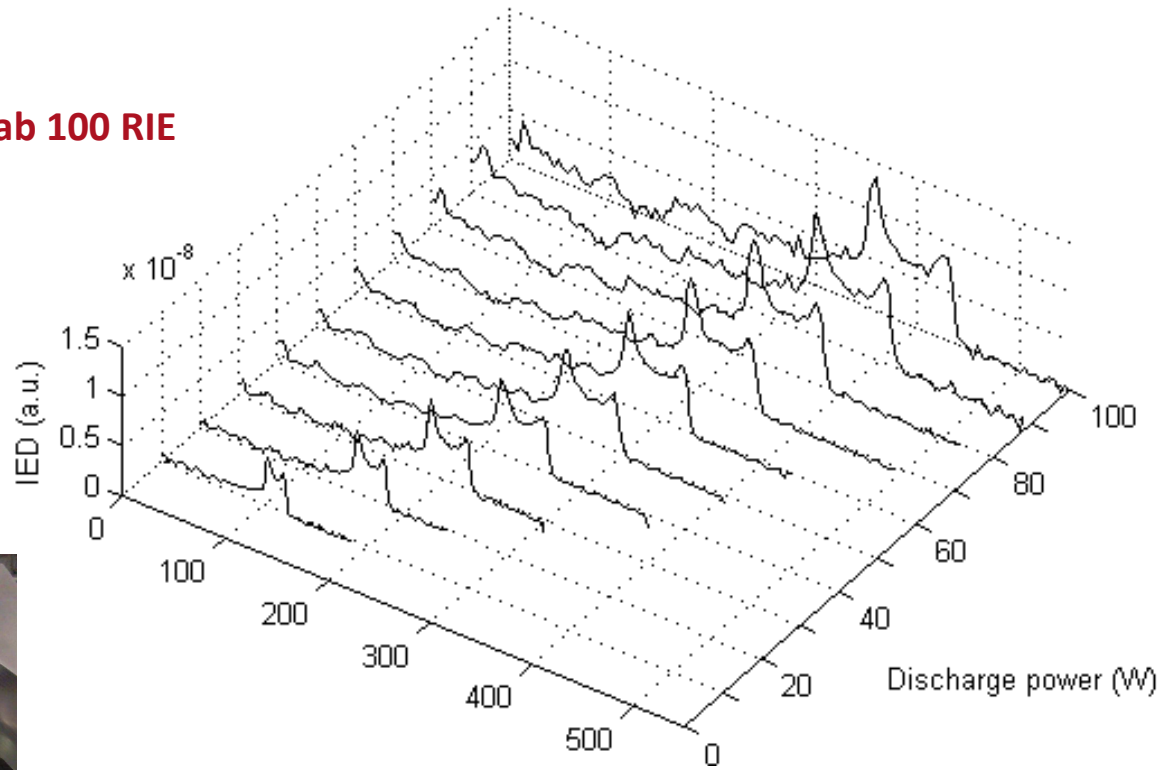
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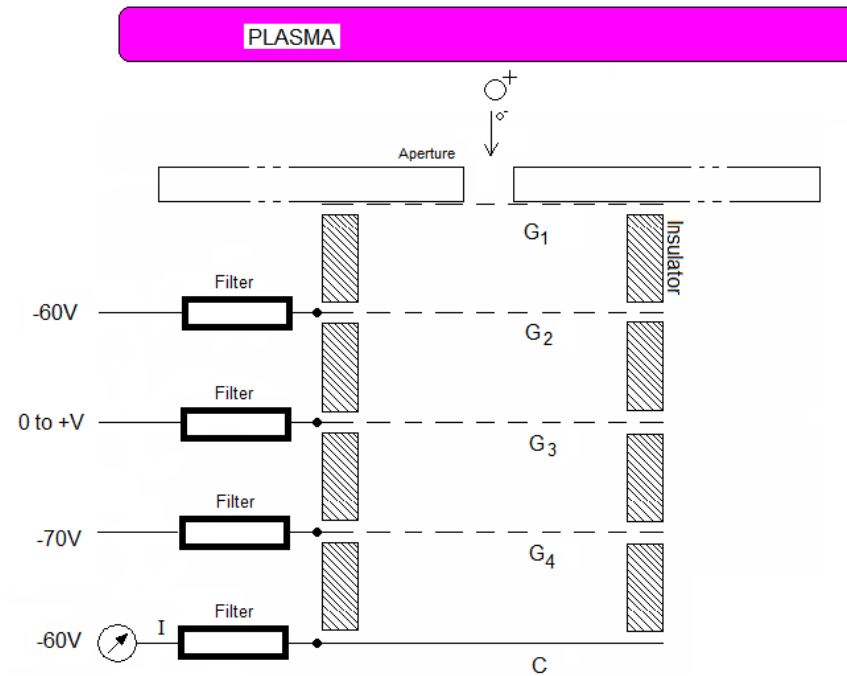
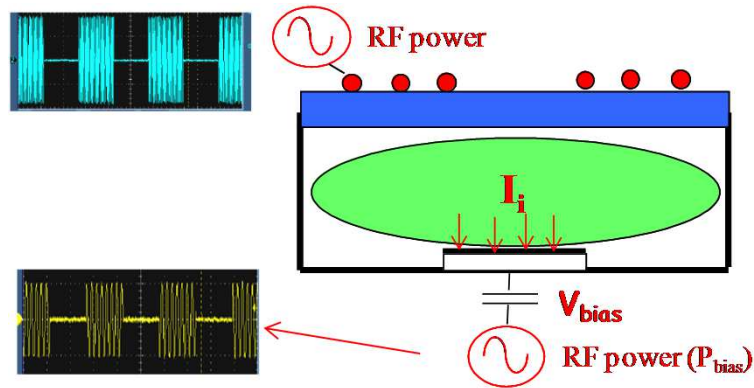
Typical results

CCP Oxford Instruments PlasmaLab 100 RIE



Pulsed RF Requirements

Pulse frequencies in kHz range



Ion flux and ion distribution function measurements in synchronously pulsed inductively coupled plasmas

Melisa Brihoum, Gilles Cunge,^{a)} and Maxime Darnon
Laboratoire des Technologies de la Microélectronique CNRS, Grenoble Cedex 9, Isere 38054, France

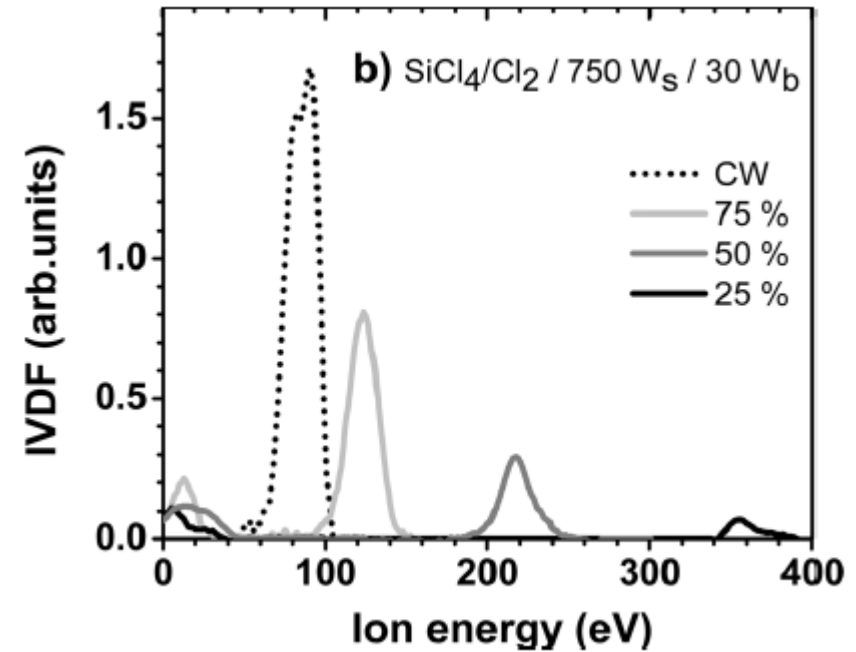
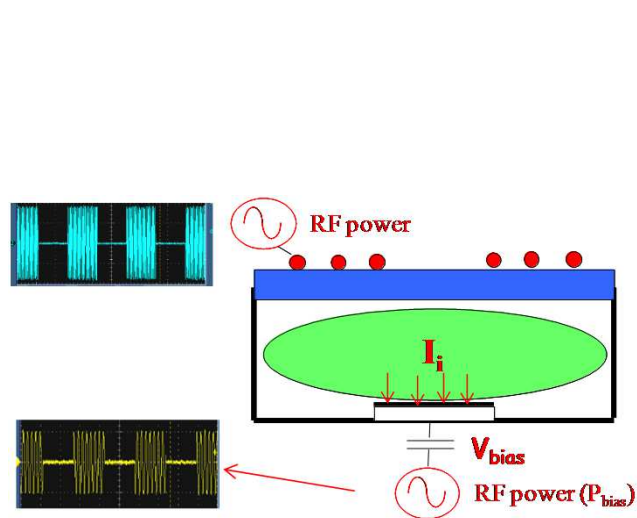
David Gahan
Impedans Ltd., Dublin 17, Ireland

Olivier Joubert
Laboratoire des Technologies de la Microélectronique CNRS, Grenoble Cedex 9, Isere 38054, France

Nicholas St. J. Braithwaite
Department of Physical Sciences, The Open University, Walton Hall, Milton Keynes MK7 6AA, United Kingdom

Pulsed RF Plasma

IEDF in synchronous pulsed plasmas (with bias power)



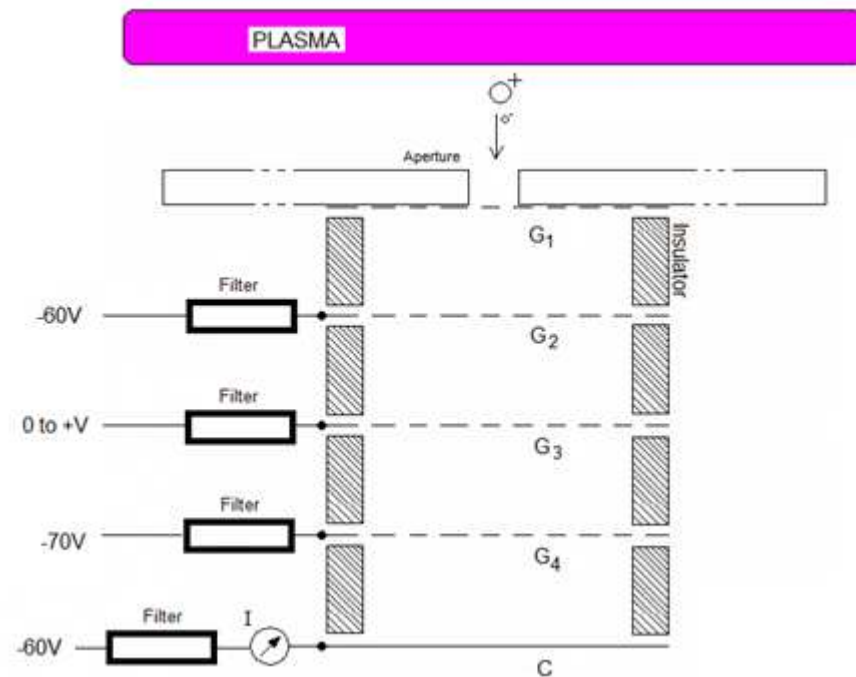
- Bi-modal IEDF (corresponding to ions from ON and OFF periods)

Ion energies accessible that are beyond the capabilities of CW ICP plasma with bias power

Time Resolved Functionality

Filtering prevents good time resolution generally

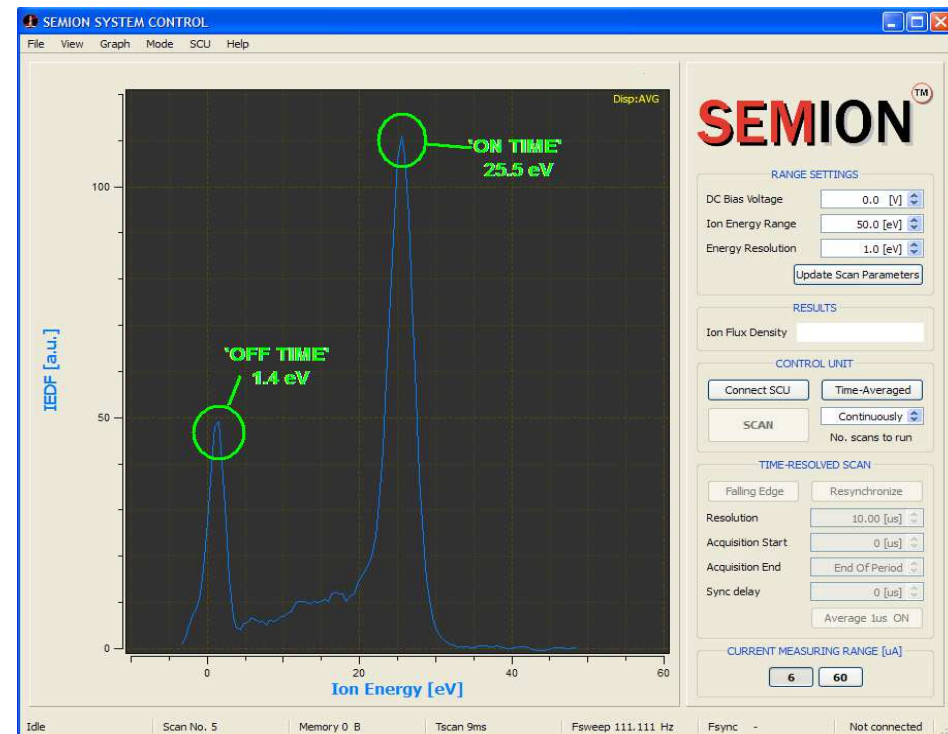
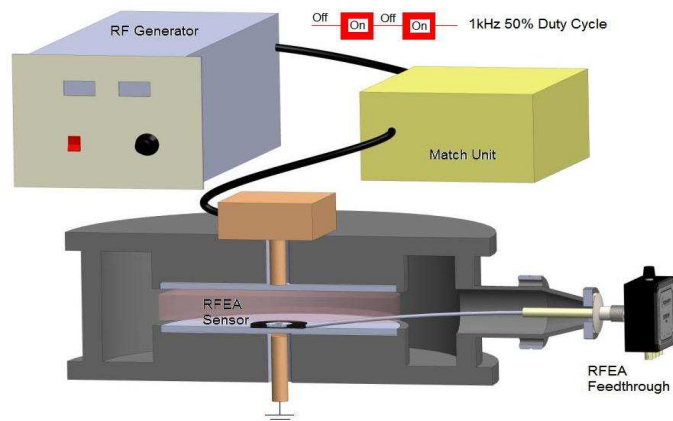
- Measurement circuit designed to sit on RF side of filter
- 1us resolution just released for pulsed RF application



Time Resolved Functionality

Pulsed CCP example

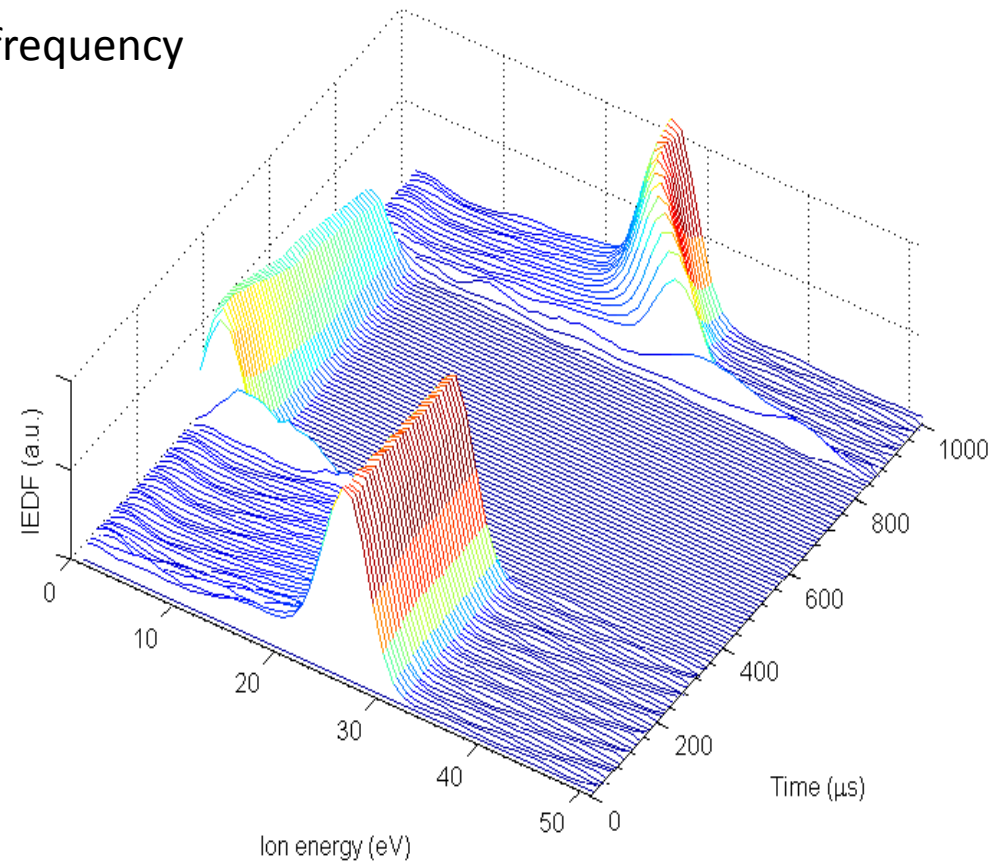
- Bottom electrode grounded (till now design only suitable for grounded or floating electrode)
- Source modulated at 1 kHz
- Square wave modulation, 50%
- Time Averaged measurement



Time Resolved Functionality

Pulsed CCP example

- Time resolved measurement
- 10 μ s resolution, 1kHz pulse frequency

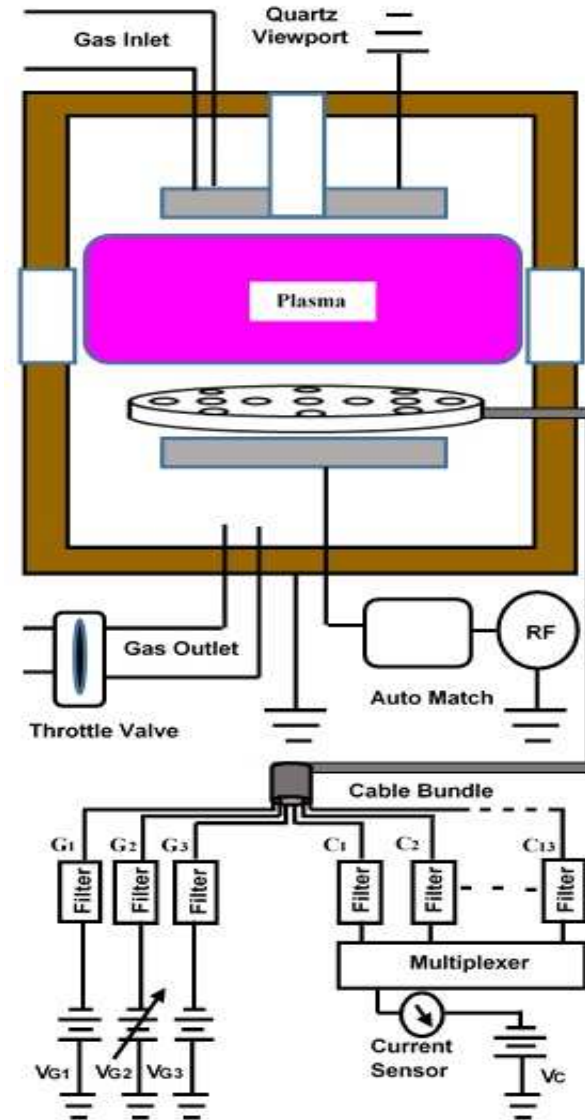


RFA with Spatial Resolution

- Measures
 - Ion Energy
 - Ion Flux
 - Temperature
 - Spatial Profile from 13 (300mm) and 17 (450mm) Different Locations
- Ion Energy Range 0 to 2500eV (5keV on request)



RFA with Spatial Resolution



A spatially resolved retarding field energy analyzer design suitable for uniformity analysis across the surface of a semiconductor wafer

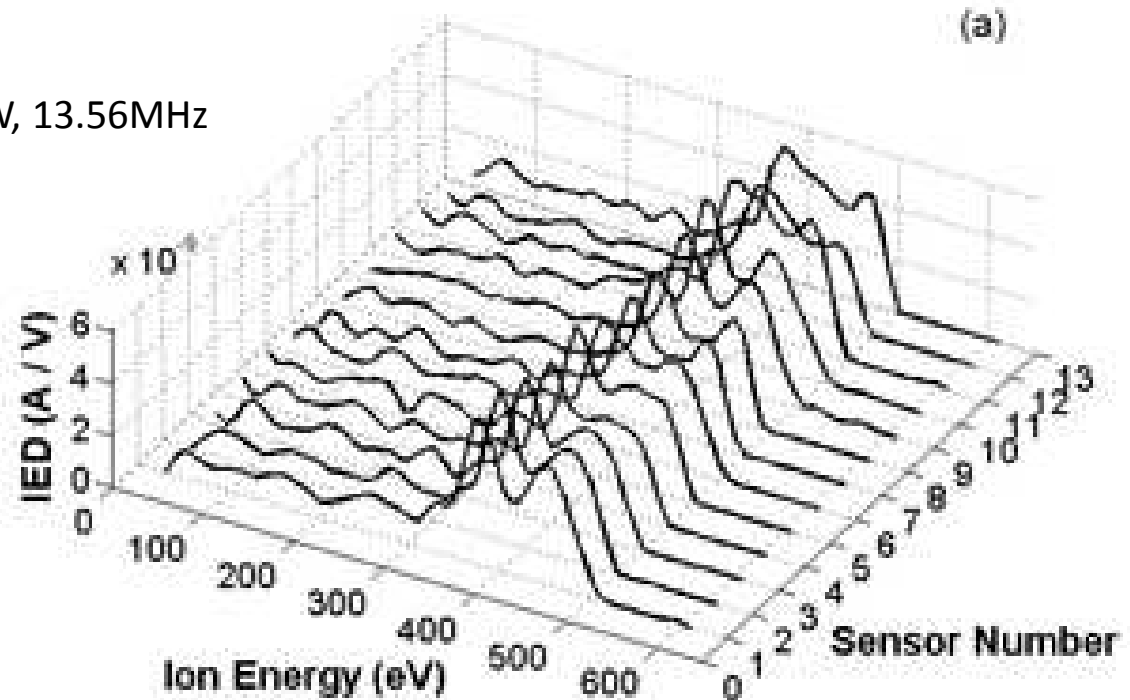
S. Sharma,^{1,2,a)} D. Gahan,^{1,b)} S. Kechkar,² S. Daniels,² and M. B. Hopkins¹

¹Impedans Ltd., Unit 8 Woodford Court, Woodford Business Park, Santry, Dublin 17, Ireland

²National Centre for Plasma Science and Technology, Dublin City University, Glasnevin, Dublin 9, Ireland

RFA with Spatial Resolution

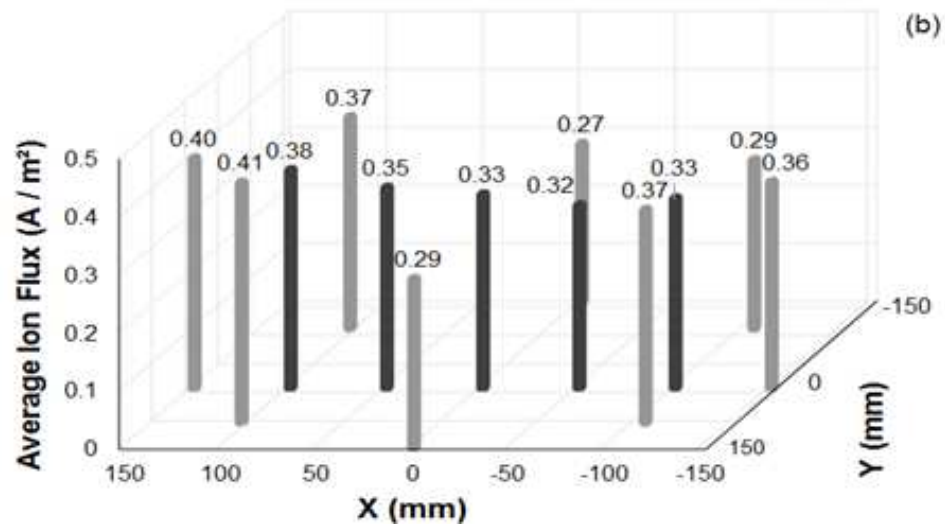
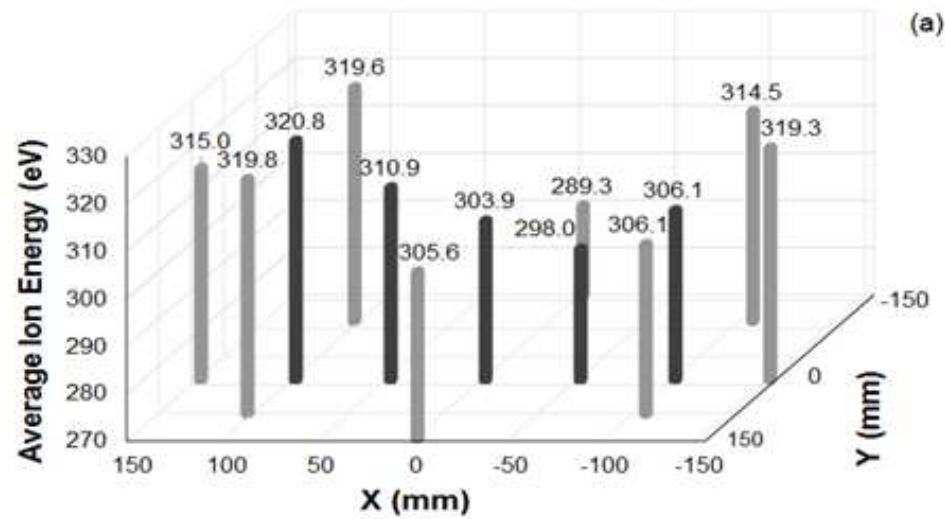
- Argon Plasma, 20mTorr, 100W, 13.56MHz



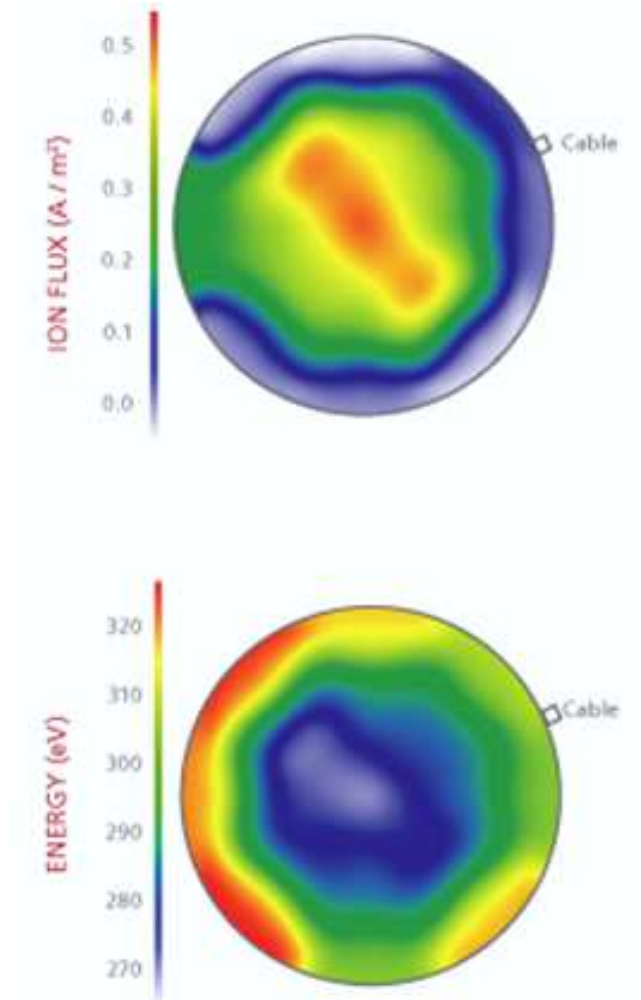
$$J_i = \left(\int_{E_{min}}^{E_{max}} IED dE \right) / AT$$

$$E_i = \left(\int_{E_{min}}^{E_{max}} E (IED) dE \right) / \left(\int_{E_{min}}^{E_{max}} IED dE \right)$$

RFA with Spatial Resolution



RFA with Spatial Resolution



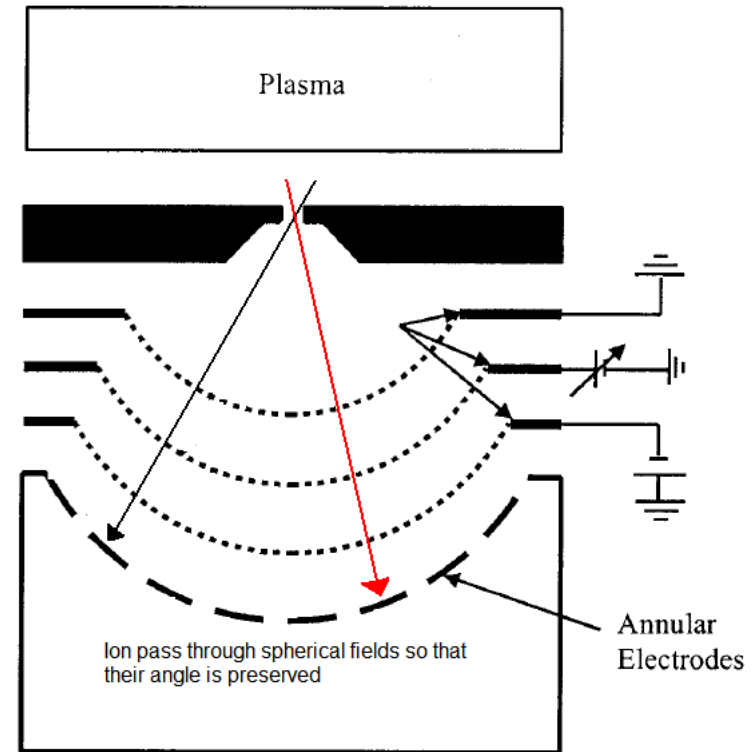
Ion Energy Distribution as a function of Angle

Important parameter for anisotropic etching

- Angular ions travel straight through the spherical fields
- Multiple detectors located at appropriate angles to collect the ion coming ions

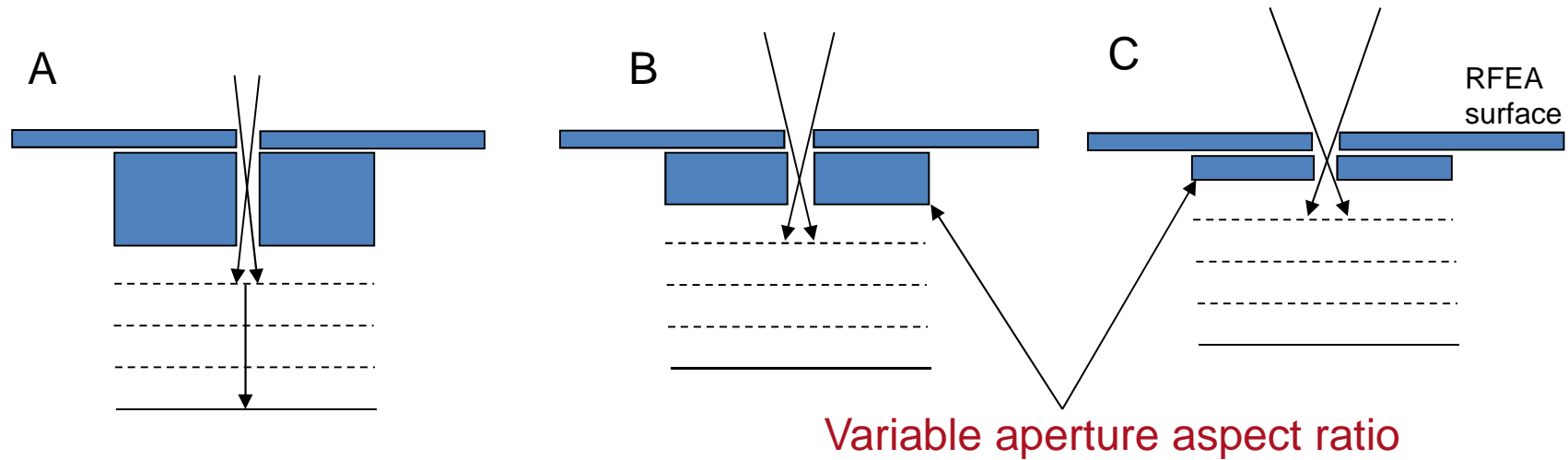
Disadvantages

- Spherical grids difficult to manufacture
- Physical depth of sensor is large (25mm)
- This limits operating pressure i.e. 25mm sensor limited to 2mTorr upper pressure range



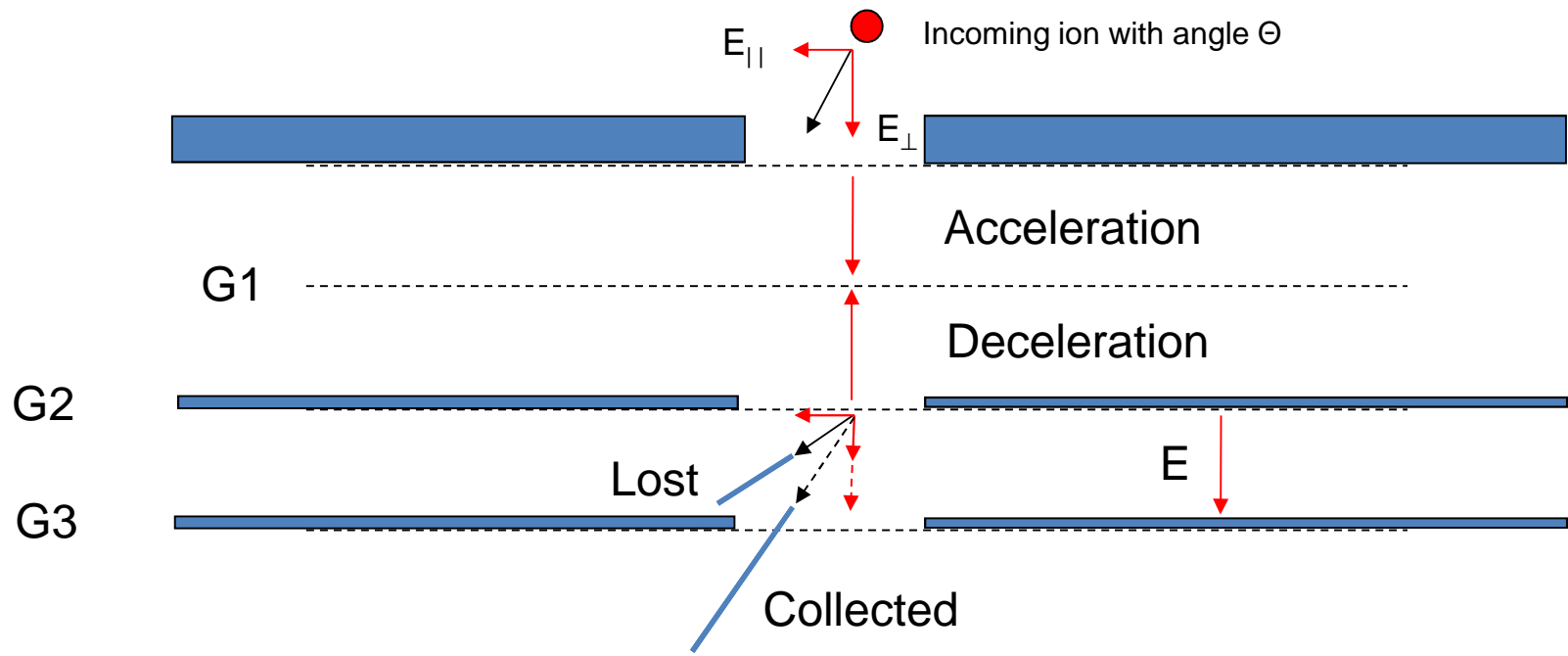
Ion Energy Distribution as a function of Angle

Additional aperture added inside standard RFEA structure



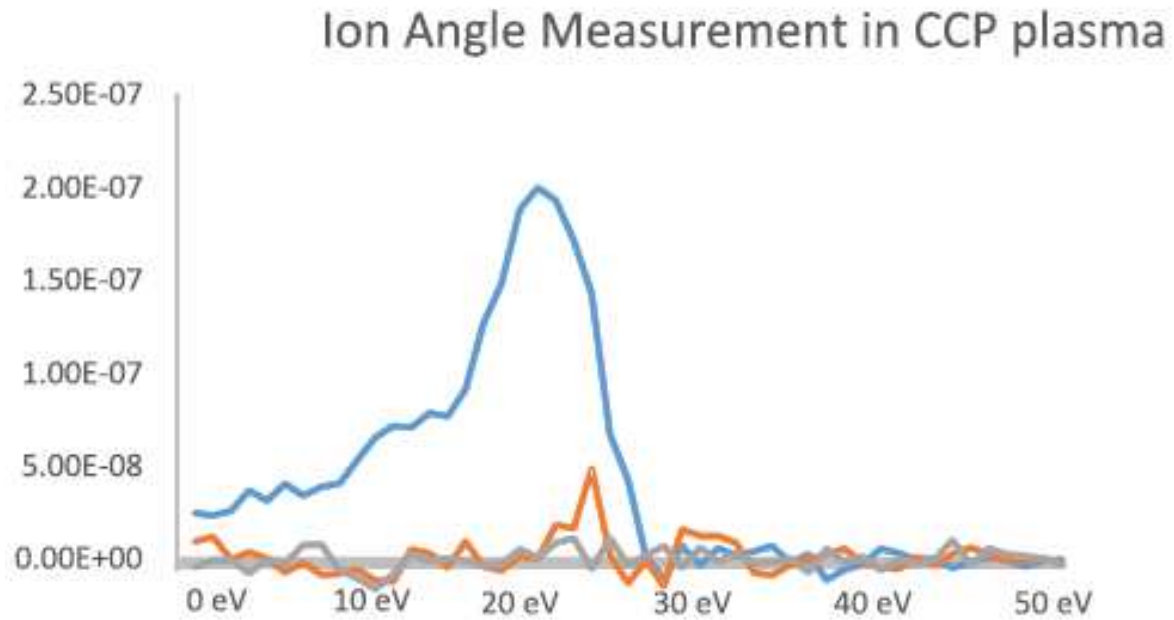
- Mechanical aspect ratio variation complicated

Ion Energy Distribution as a function of Angle



- G2 selects the Ion energy
- Potential of G3 varied wrt G2 to scan angular distribution
- Energy and angle in integral form – multiple derivatives required

Ion Energy Distribution as a function of Angle



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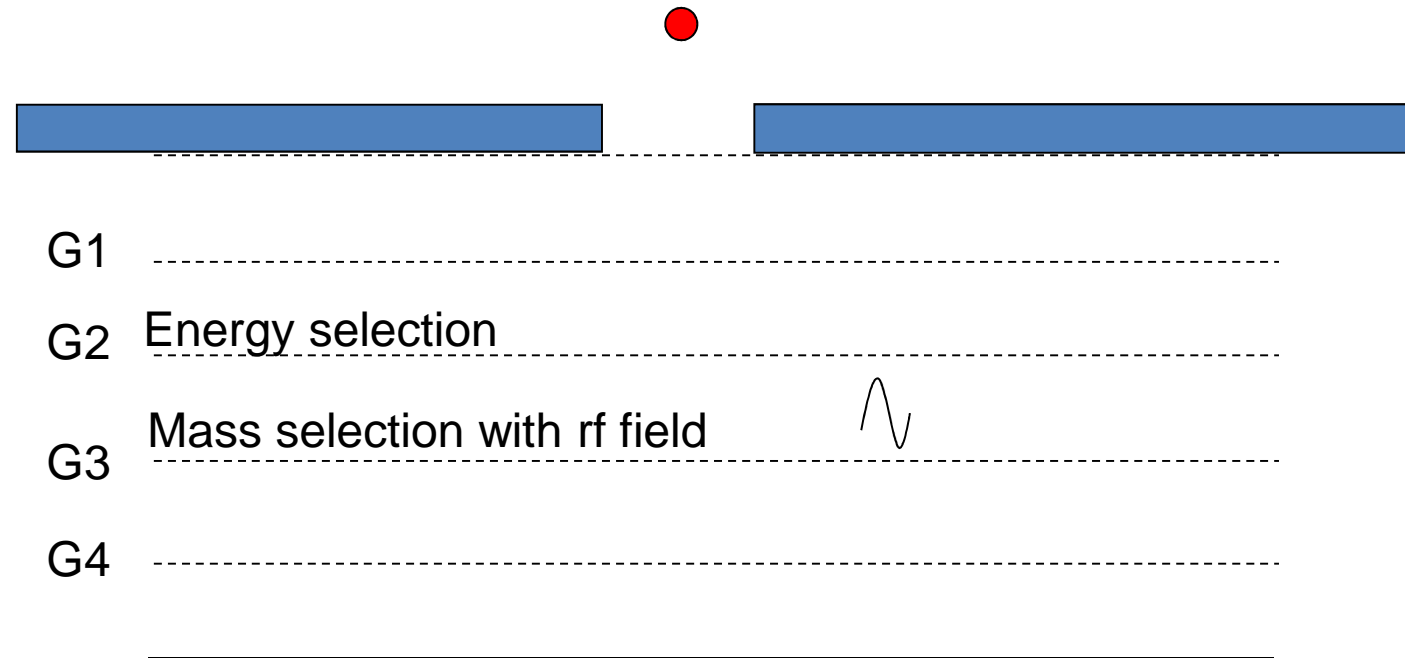
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- Wireless sensors

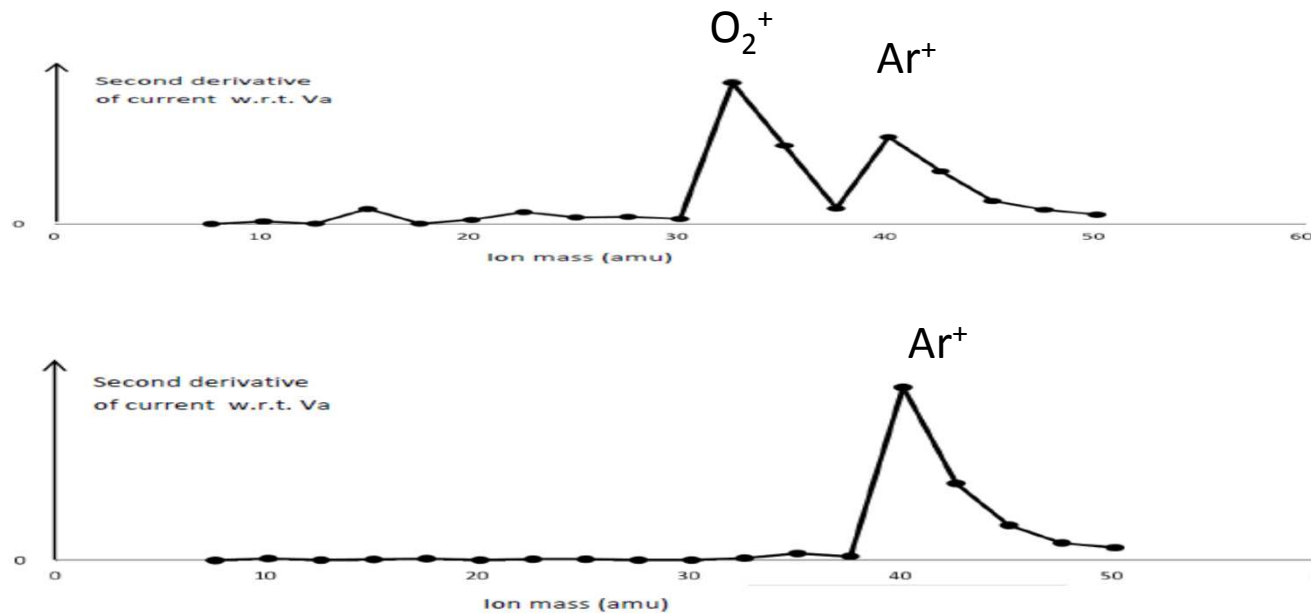
Ion Mass Resolution



- G2 selects the Ion energy
- RF field between G2 and G3, scan over suitable frequency range
- Energy of ions dispersed, proportional to ion mass
- Energy and mass in integral form – complex numerical solutions required

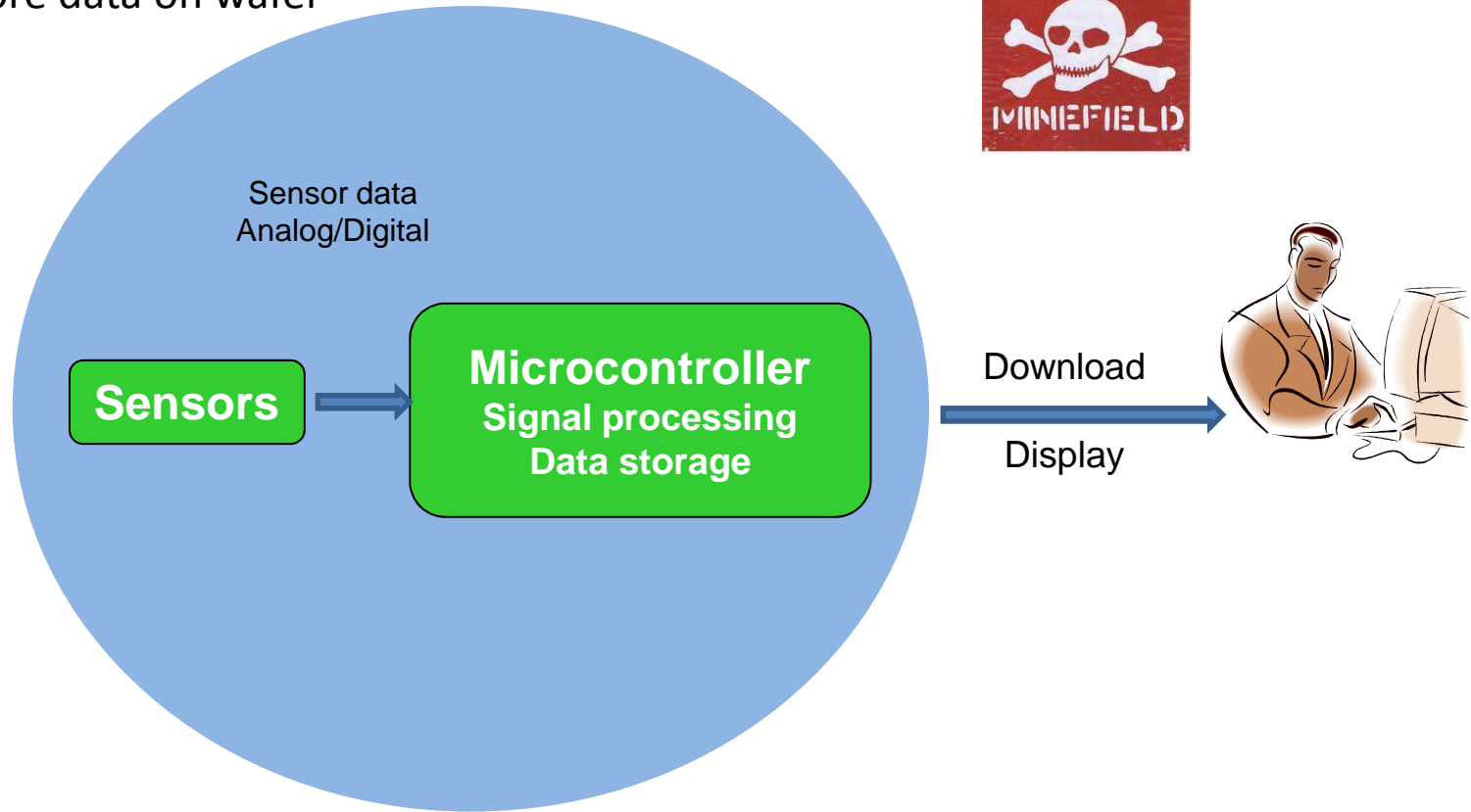
Ion Mass Resolution

Initial data from an Argon and Argon Oxygen plasma shows that Semion mass can currently resolve to better than 5 AMU. The first product will be released in late 2014.



Wireless Sensors

KLA On Wafer Approach
Measure and store data on wafer



IP Minefield

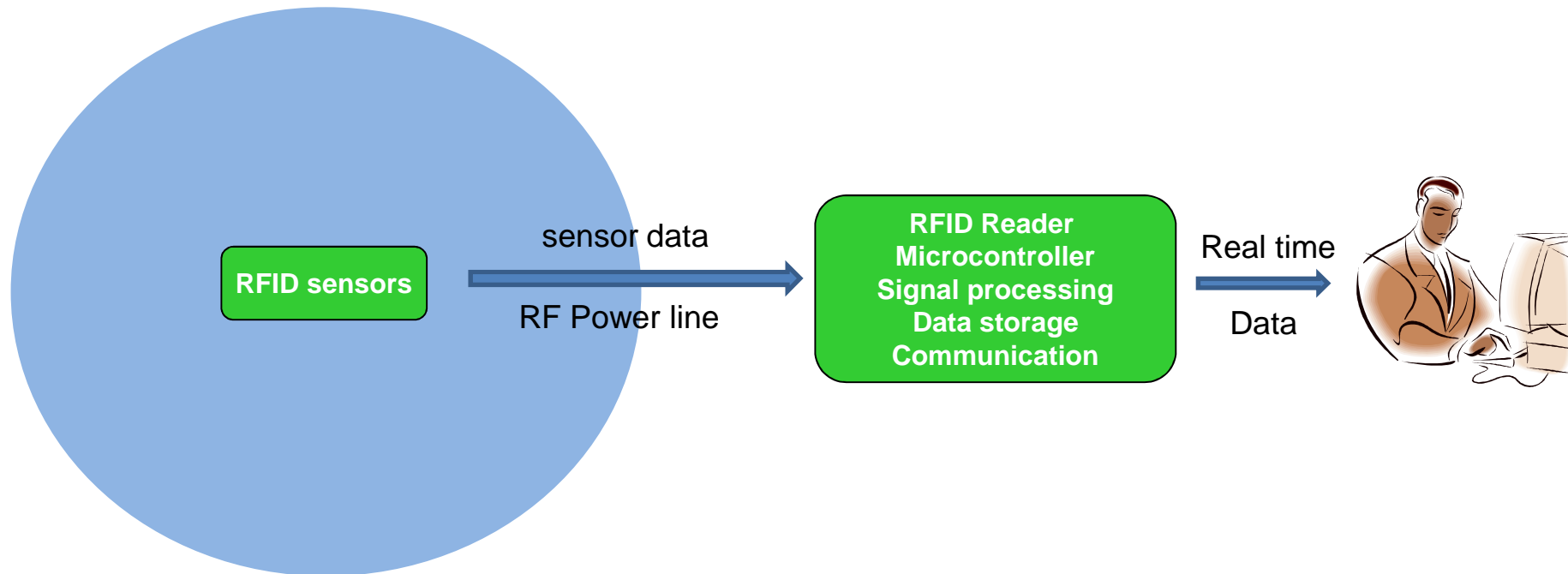


Wireless Sensors

Impedans Approach

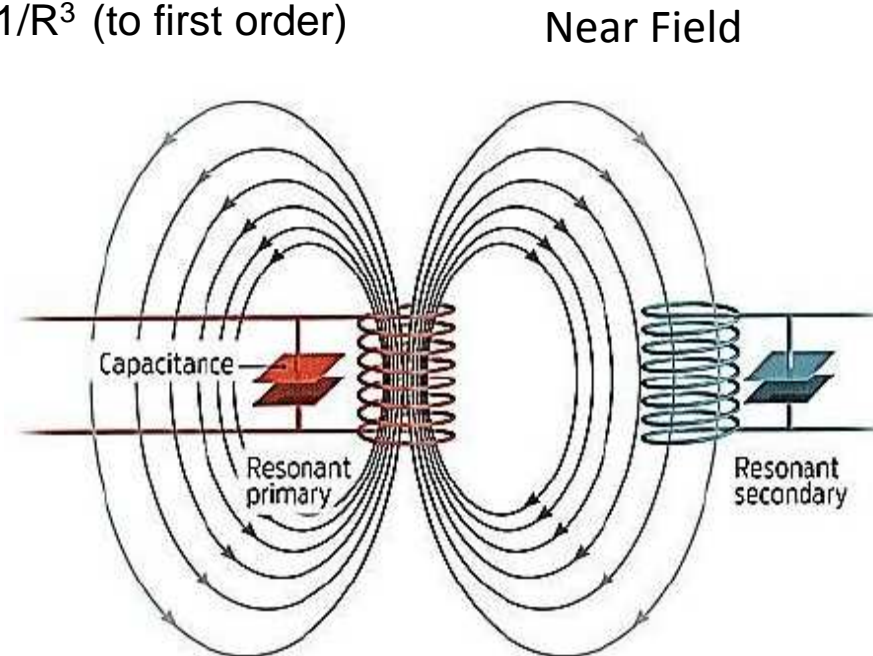
Patent **WO 2011/131769 A1**

Transmit data from RFID sensor to external reader on RF power line



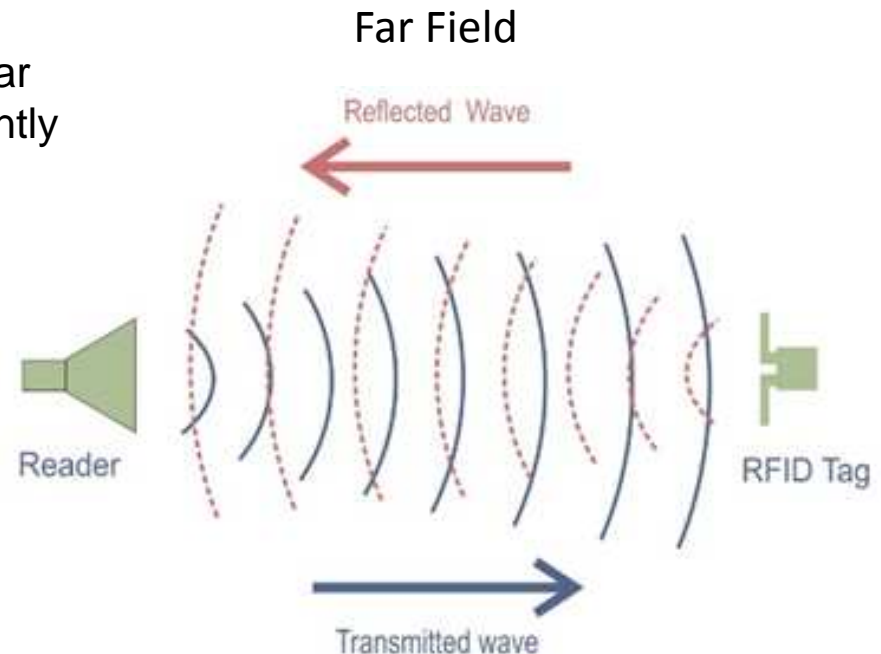
Wireless Sensors

- RFID Tags
- Near field (13.56MHz typically)
- Inductive coupling of tag to magnetic field circulating around antenna (like a transformer).
- Varying magnetic flux induces current in tag.
- Modulate tag load to communicate with reader
- Field energy decreases proportionally to $1/R^3$ (to first order)



Wireless Sensors

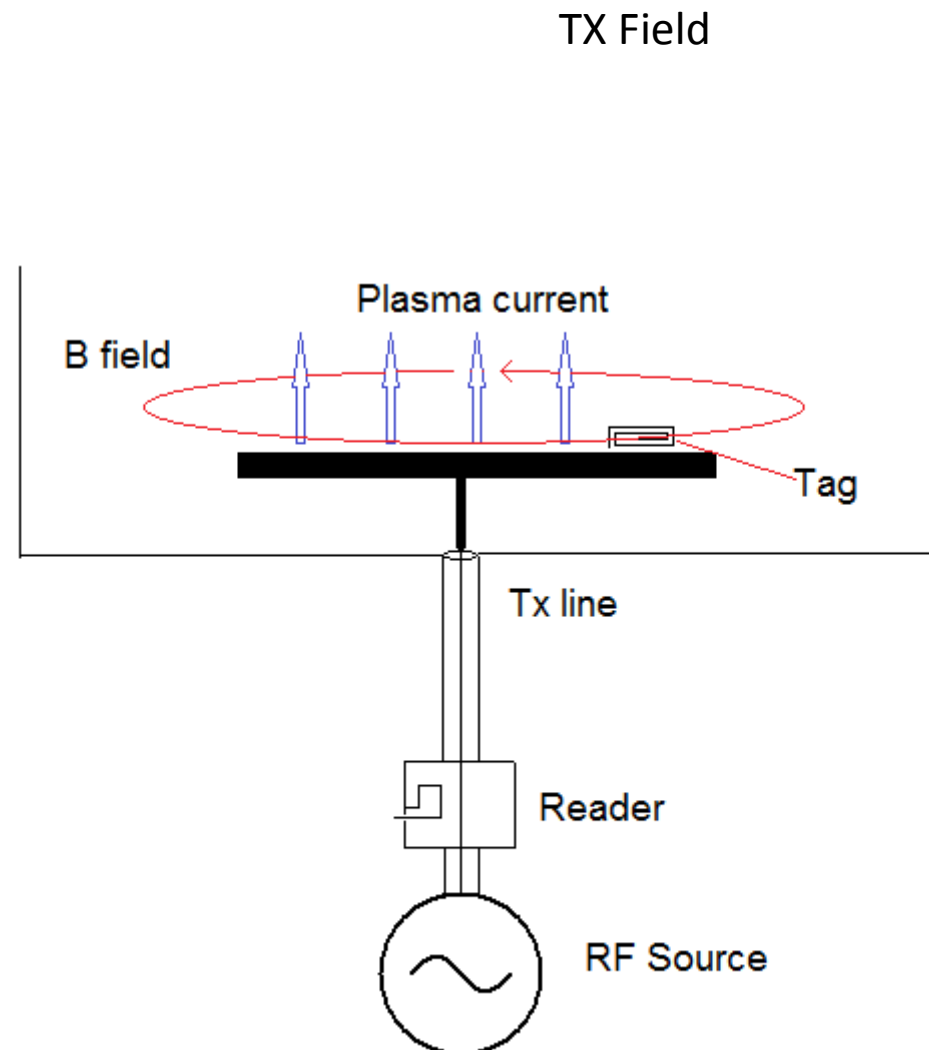
- RFID Tags
- Far field (UHF, microwave):
- Backscatter.
- Modulate back scatter by changing antenna impedance.
- Field energy decreases proportionally to $1/R$.
Boundary between near and far field: $R = \text{wavelength}/2\pi$ so, once you have reached far field, lower frequencies will have lost significantly more energy than high frequencies



Wireless Sensors

- RFID Tags
- Transmission Line coupling

- Energy is coupled into transmission line and data transmitted back via line.
- No loss of field energy over long distances.
- Similar to near field
- Primarily inductive coupling.
- Reader does not need to be source of RF energy.
- Tags embedded in wafer



Wireless Sensors are the Future

Impedans will engage with a strategic partner to productize the wireless wafer solution in the Semiconductor market.

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